

7th PISA MEETING
F. COSTANTINI
PISA UNIV. & INFN

THE NA48 LIQUID KRYPTON CALORIMETER

FIRST OPERATION RESULTS

NA48 COLLABORATION

CAGLIARI - CAMBRIDGE - CERN - DUBNA - EDINBURGH
FERRARA - FIRENZE - MAINZ - ORSAY - PERUGIA - PISA
SIEGEN - SACLAY - TORINO - VIENNA - WARSAW

OUTLINE

- PHYSICS REQUIREMENTS ON THE CALORIMETER
- CALORIMETER STRUCTURE & FEED ELECTRONICS
- PRELIMINARY PERFORMANCES COMPARED TO THE PROTOTYPE ONES:

ENERGY, POSITION, TIME RESOLUTIONS

PHYSICS AIM

- THE NA48 EXP.T IS DESIGNED TO MEASURE THE DIRECT ~~CP~~ OBSERVABLE R: \searrow

$$\text{Re}(\varepsilon'/\varepsilon) = \frac{1}{6} (1-R) \leftarrow R = \frac{\Gamma(K_L \rightarrow \pi^0 \pi^0)}{\Gamma(K_S \rightarrow \pi^0 \pi^0)} \cdot \frac{\Gamma(K_S \rightarrow \pi^+ \pi^-)}{\Gamma(K_L \rightarrow \pi^+ \pi^-)}$$

- A 10^{-3} DEVIATION FROM UNITY IN DOUBLE RATIO R DETERMINES A $\sim 2 \cdot 10^{-4}$ VARIATION ON $\text{Re}(\varepsilon'/\varepsilon)$
- THE MAIN REQUIREMENTS FOR THE E.M. CALORIMETER USED TO RECONSTRUCT $K \rightarrow \pi^0 \pi^0 \rightarrow 4\gamma$ DECAYS ARE:
 - $\sigma(E)/E \sim 1\% @ 10 \text{ GeV} + \text{CONSTANT TERM} \lesssim 0.5\%$
 - POSITION RESOLUTION $\sim 1 \text{ mm}$ IN X, Y
 - TIME RESOLUTION $\lesssim 0.5 \text{ ns}$ FOR K_S IDENTIFIC.
 - SINGLE RATE CAPABILITY $\sim 1 \text{ MHz}$ TO ACHIEVE THE REQUIRED STATISTICS OF $10^6 K_L \rightarrow \pi^0 \pi^0$
 - TRANSVERSE SCALE ACCURACY OF $0.1/1000 \text{ mm}$ TO CONTROL SYSTEMATICS ERROR FROM ENERGY SCALE DIFFERENCE BTW $\pi^0 \pi^0$ AND $\pi^+ \pi^-$ DECAYS.
- THE PHOTON RANGE OF INTEREST IS $\sim 5 \div 100 \text{ GeV}$

REQUIREMENTS ON CALORIMETER :

ENERGY AND POSITION RESOLUTIONS

- THE K DECAY VERTEX POSITION ALONG THE BEAM LINES $K \rightarrow 2\pi^0 \rightarrow 4\gamma$ IS MEASURED BY THE 4 SHOWER ENERGIES AND POSITIONS IN THE CALORIMETER

$$\rightarrow \quad Z_{VTX} = \frac{1}{m_K} \left\{ \sum_{i,j < i} E_i E_j \left[(x_i - x_j)^2 + (y_i - y_j)^2 \right] \right\}^{1/2}$$

- THE ENERGY AND POSITION RESOLUTIONS
(AND THEIR UNIFORMITY!)
ALL OVER THE WHOLE CALORIMETER SURFACE

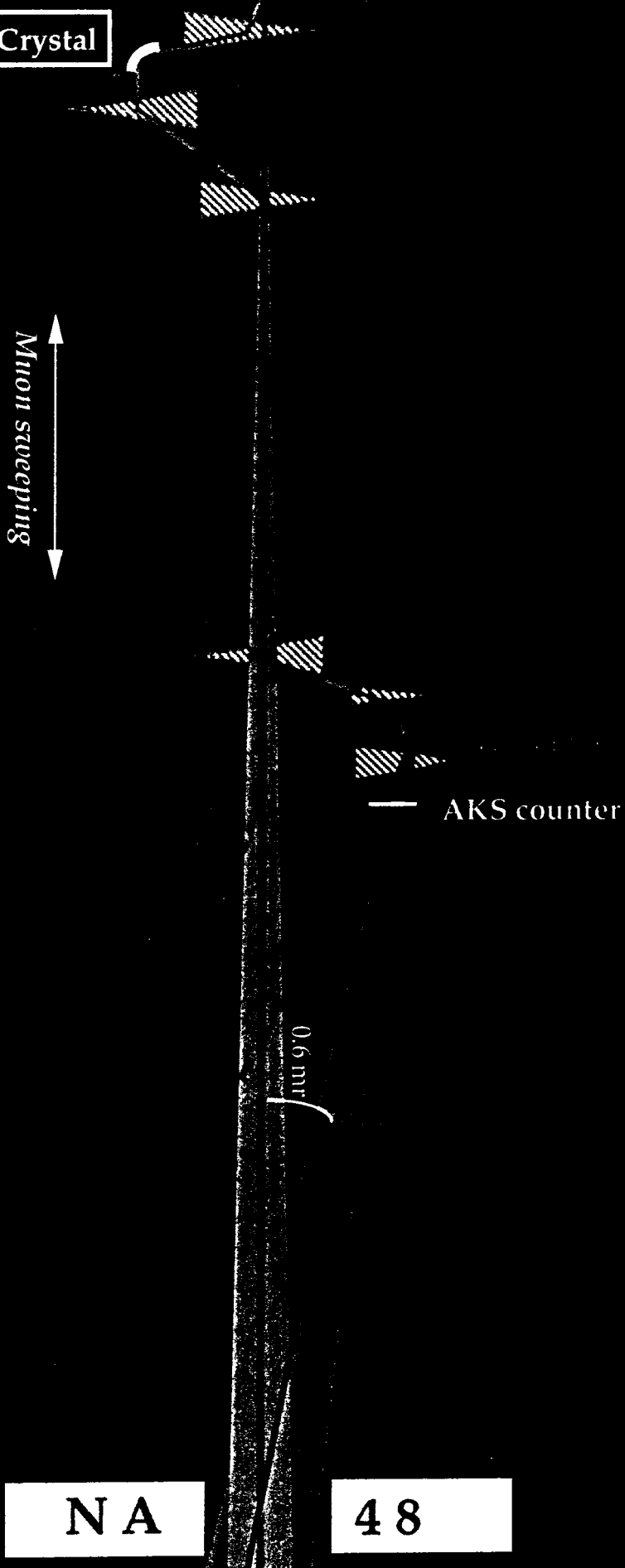
DETERMINE THE ERROR ON Z_V

- AN ERROR OF $\Delta Z_V / Z_V \approx 2 \cdot 10^{-4}$ PRODUCES AN ERROR ON $\Delta \epsilon' / \epsilon \approx 10^{-4}$

(FIDUCIAL REGION ON Z_V : $110 \text{ m} \pm 6$)

- A GOOD ENERGY RESOLUTION MINIMIZES ALSO THE BACKGROUND $K_L \rightarrow 3\pi^0$ CONTRIBUTION (WHEN ONLY 4 γ 'S ARE DETECTED) TO THE $K_L \rightarrow 2\pi^0$ SIGNAL.
(3-rd MOST IMPORTANT SOURCE OF ERROR)

THE SIMULTANEOUS K_L AND K_S BEAMS

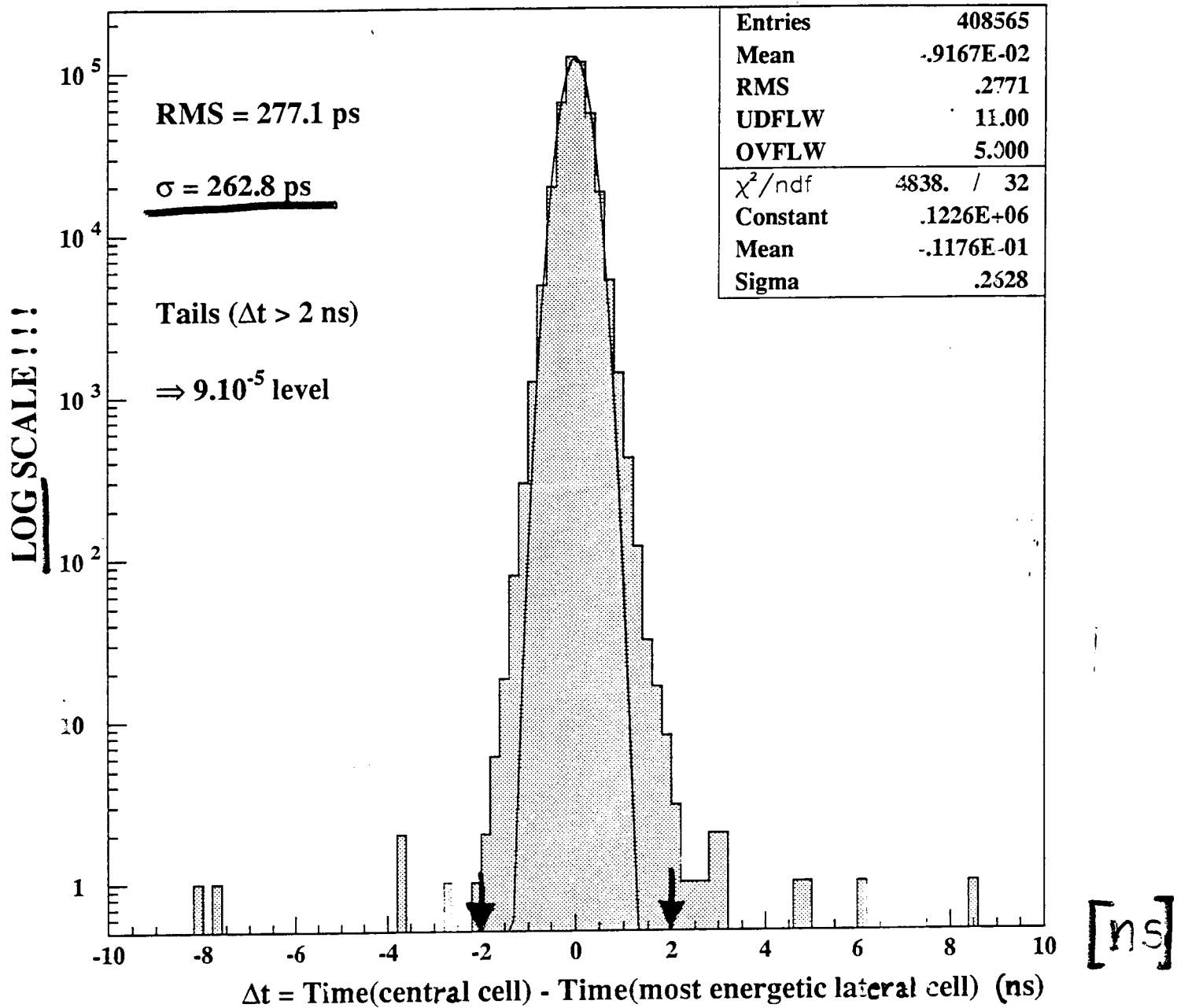


2) REQUIREMENTS ON CALORIMETER:

THE TIME RESOLUTION

- THE TIMING INFORMATION FROM THE CALORIMETER PROVIDES, IN CONJUNCTION WITH THE TIMING FROM THE K_S TAGGER, THE WAY TO TELL A K_S NEUTRAL DECAY FROM A K_L ONE.
- A GOOD CALORIMETER TIME RESOLUTION IS THEREFORE VITAL FOR THE EXPERIMENT
- A $\sigma(t)$ OF 260 ps HAS BEEN OBTAINED FOR 50 GeV electrons IN 1996
(SEE Sabine CRÉPÉ TALK)
OVER THE CALORIMETER CENTRAL REGION
EQUIPPED WITH SINGLE CELL FADC READ-OUT
i.e. 384 channels

LKr calorimeter time resolution (50 GeV e⁻)

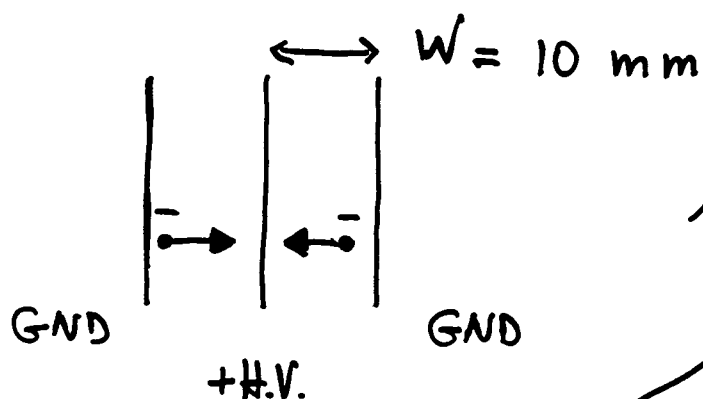


THE CALORIMETER STRUCTURE

- A TOWER STRUCTURE IS OBTAINED BY ~ 13500 CELLS
($2 \times 2 \text{ cm}^2$) $\times 120 \text{ cm}$ ($\sim 26 X_0$ DEPTH)

→ A SINGLE CELL GETS AT MOST $\sim 50\%$ OF SHOWER

- EACH CELL IS FORMED BY TWO EXTERNAL GROUND RIBBONS AND BY A CENTRAL ONE AT +H.V.



$$i(t) = i_0 \left(1 - \frac{t}{T_D}\right) e^{-t/\tau}$$

if LKr life-time $\tau \gg T_D$
this can be neglected.

In '96 $\tau \gtrsim 40 \mu\text{s}$

$T_D = 3.7 \mu\text{s}$ (1.5 kV)

INITIAL CURRENT READ-OUT METHOD

$$i_0 = Q_{\text{ION}} \frac{V_{\text{DRIFT}}}{\text{Width}}$$

↓
 \propto ENERGY

$\sim 50 \mu\text{m}/10\text{mm}$

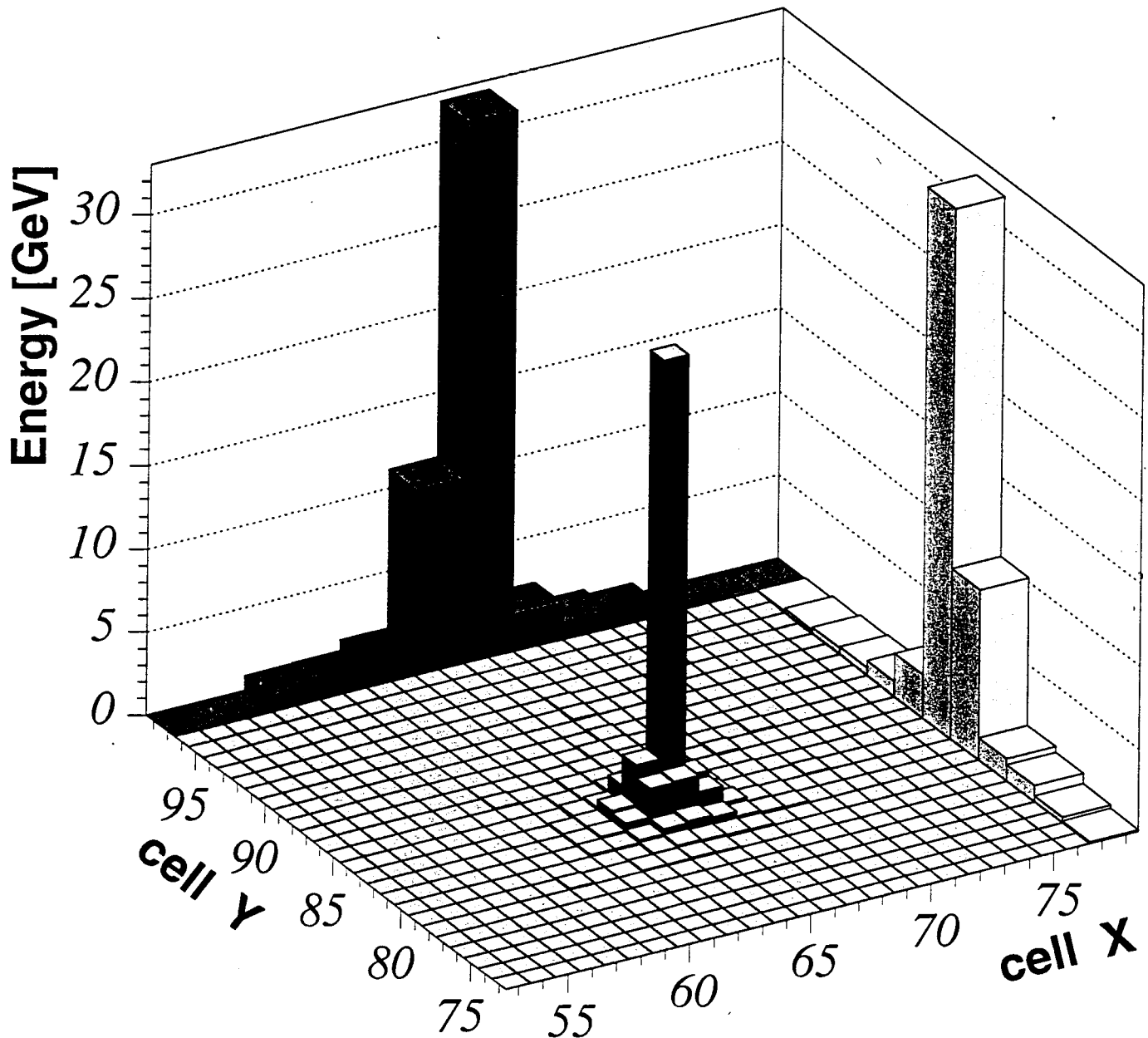
Geometrical accuracy

LKr Uniformity (space & time)

(e.g. $\Delta V_{\text{DRIFT}} / \Delta T \sim -0.9\% / \text{K}$)

NA48 LKr

50 GeV e^-



- X AND Y PROJECTIONS (FACTOR 2 LESS GRANULARITY) ARE USED FOR TRIGGERING ON K NEUTRAL DECAYS

(See I. MIKULEC)

THE CALORIMETER STRUCTURE (CONT.)

- TO COPE WITH THE STRINGENT REQUIR.TS ON CELL WIDTH UNIFORMITY ($\sim 0.5\%$)

RIBBON POSITIONS ARE FIXED BY A SET OF 5

→ SPACER PLATES. THEY ARE PLACED EVERY 20 cm

- SPACERS ARE DISPLACED GIVING A ± 50 mrad

→ LONGITUDINAL 'ZIG-ZAG' TO THE RIBBONS.

- THIS ACCORDEON SHAPE REDUCES TO $\sim \pm 0.5\%$

→ A SMALL DROP IN RESPONSE UNIFORMITY

ACROSS THE CELL, WHEN THE SHOWER CORE HITS THE CENTRAL ANODE RIBBON

- A PROJECTIVE GEOMETRY POINTING TO

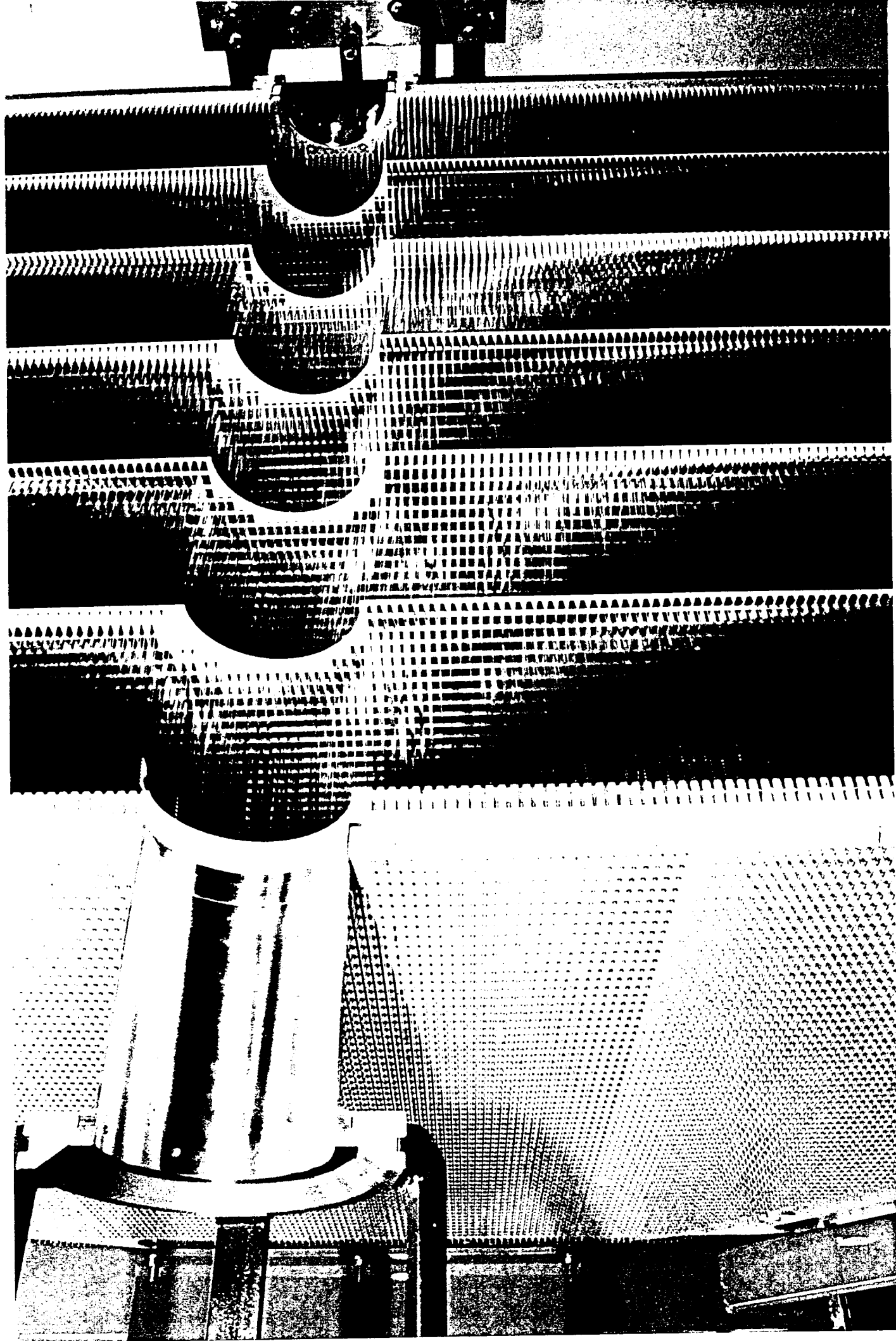
~ 110 m UPSTREAM, IS OBTAINED LINEARLY

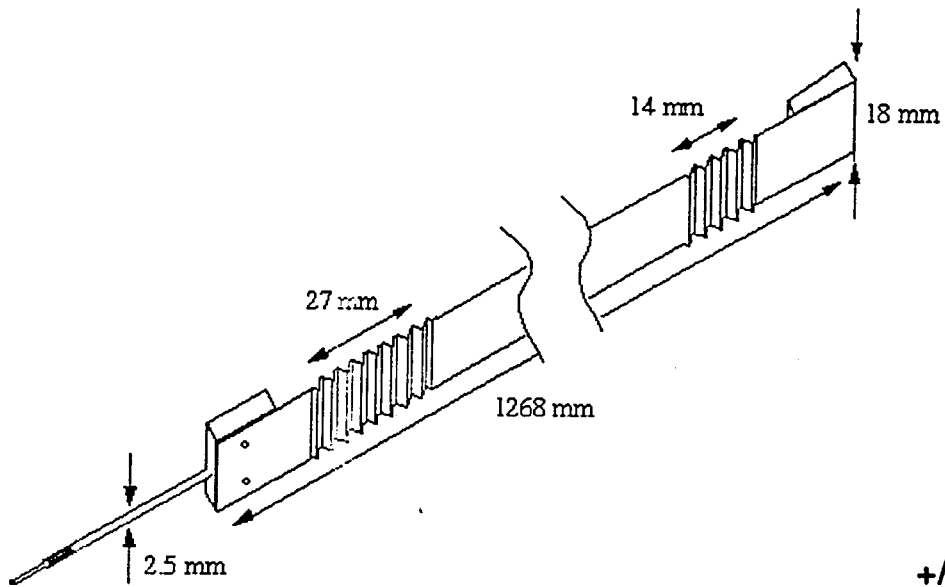
INCREASING THE CELL TRANSVERSE SIZE

(IN X AND Y) FROM THE FRONT PLATE,

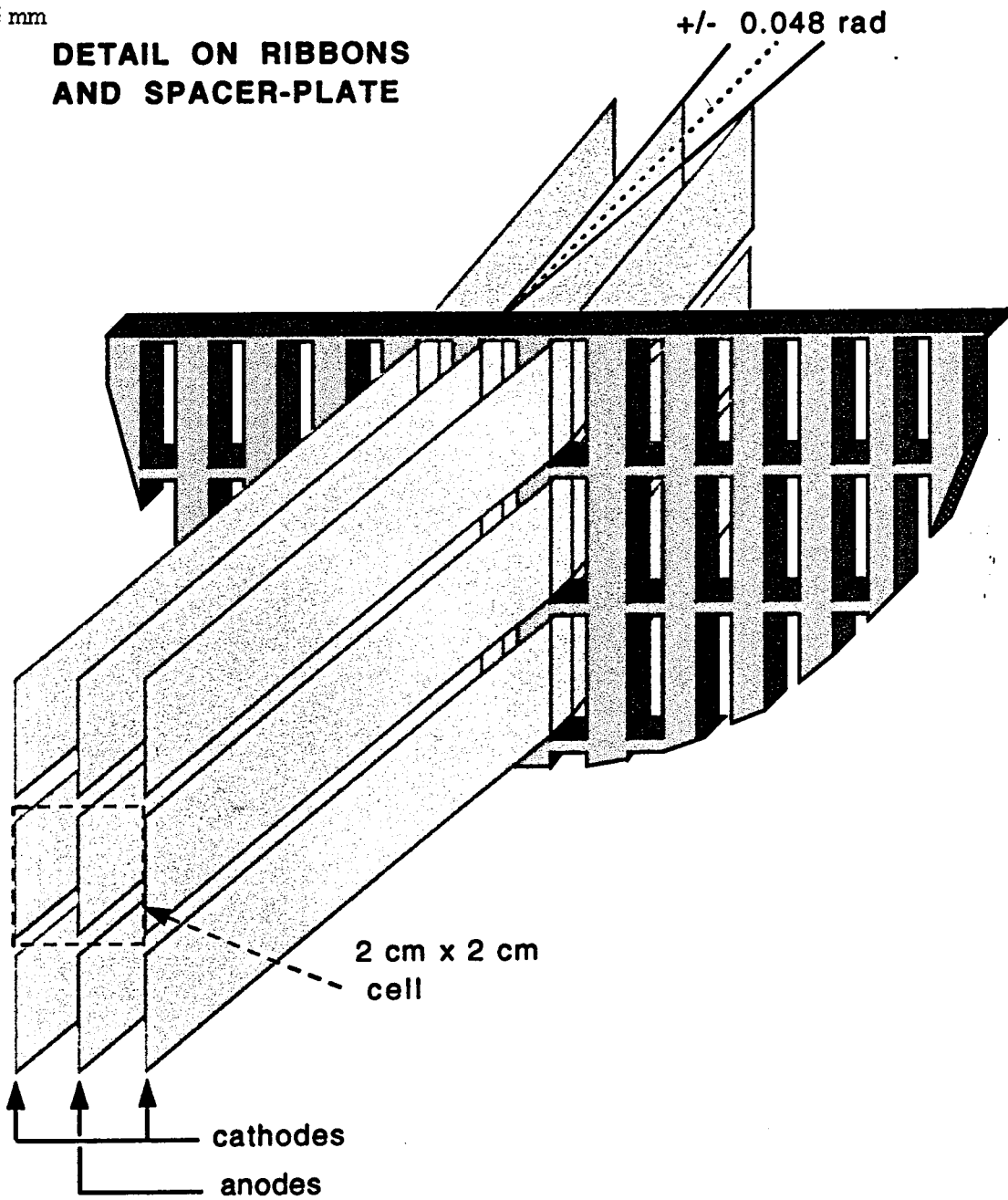
ADDING UP TO $+1.1\%$.

- THE SHOWER RESPONSE UNIFORMITY BOTH ON THE IMPACT POINT RADIUS AND ON THE DEPTH OF SHOWER MAXIMUM, IS IMPROVED IN THIS WAY.

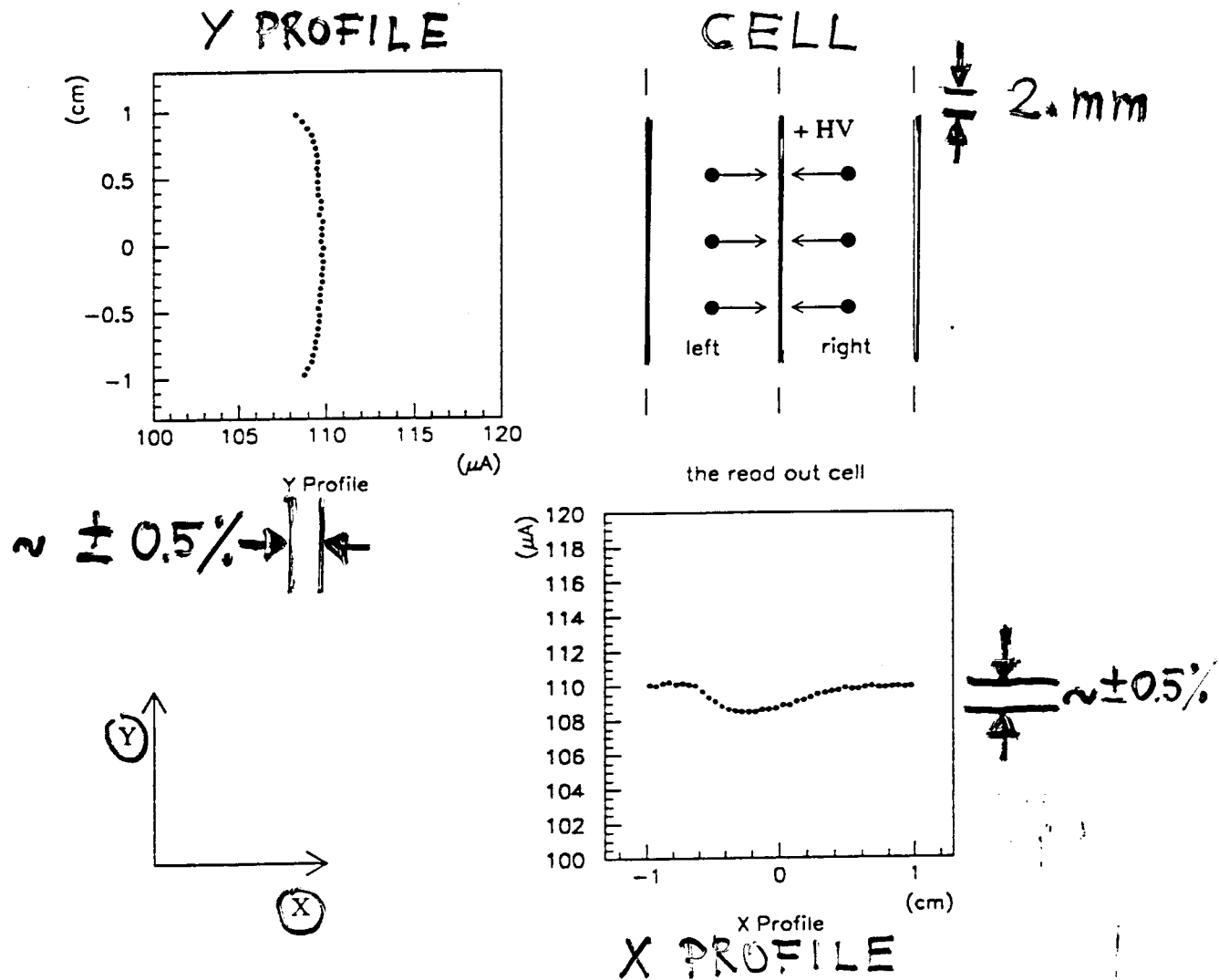




**DETAIL ON RIBBONS
AND SPACER-PLATE**



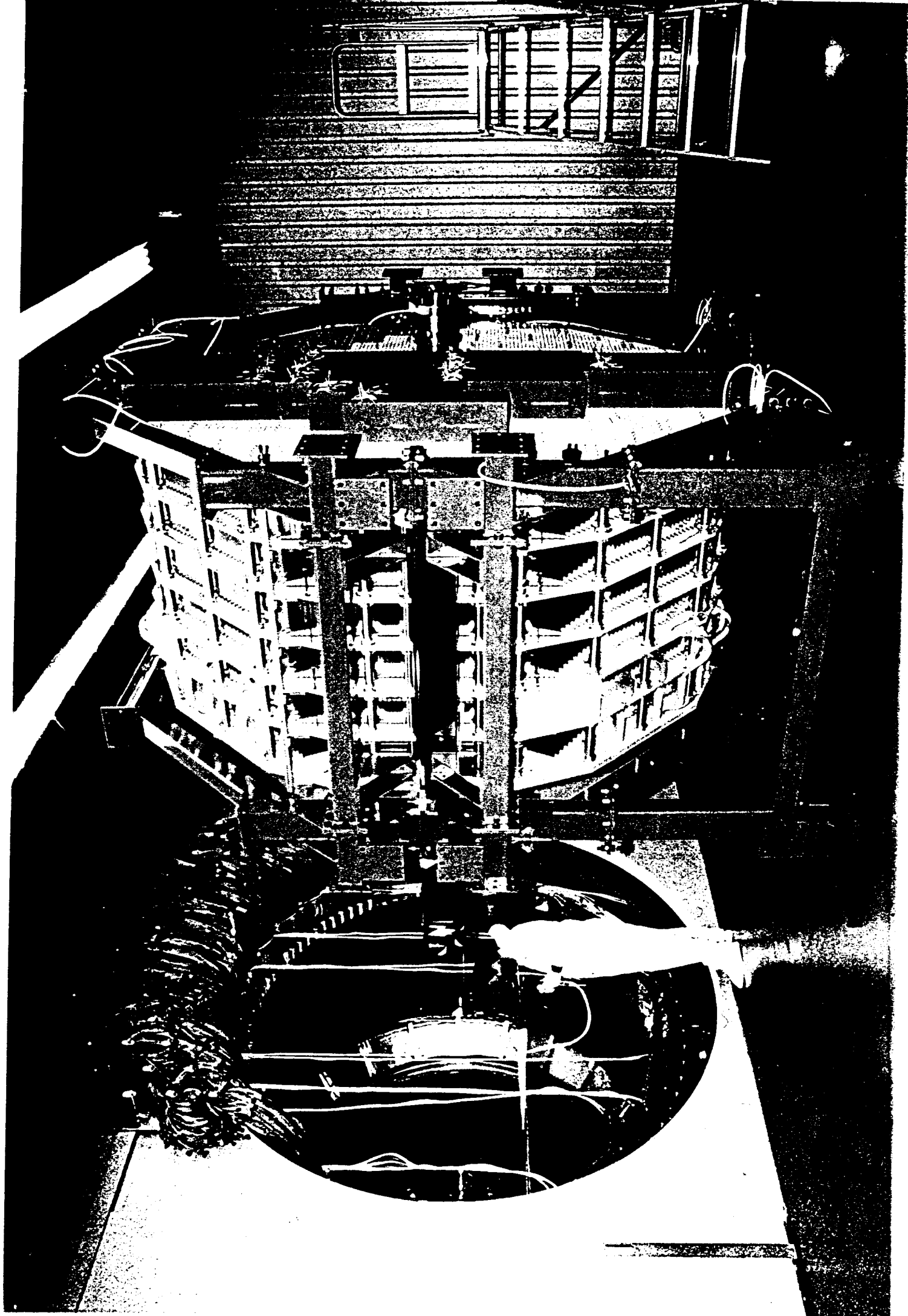
• UNIFORMITY INSIDE CELLS



- UNIFORMITY CORRECTIONS ARE IDENTICAL FOR ALL CELLS.

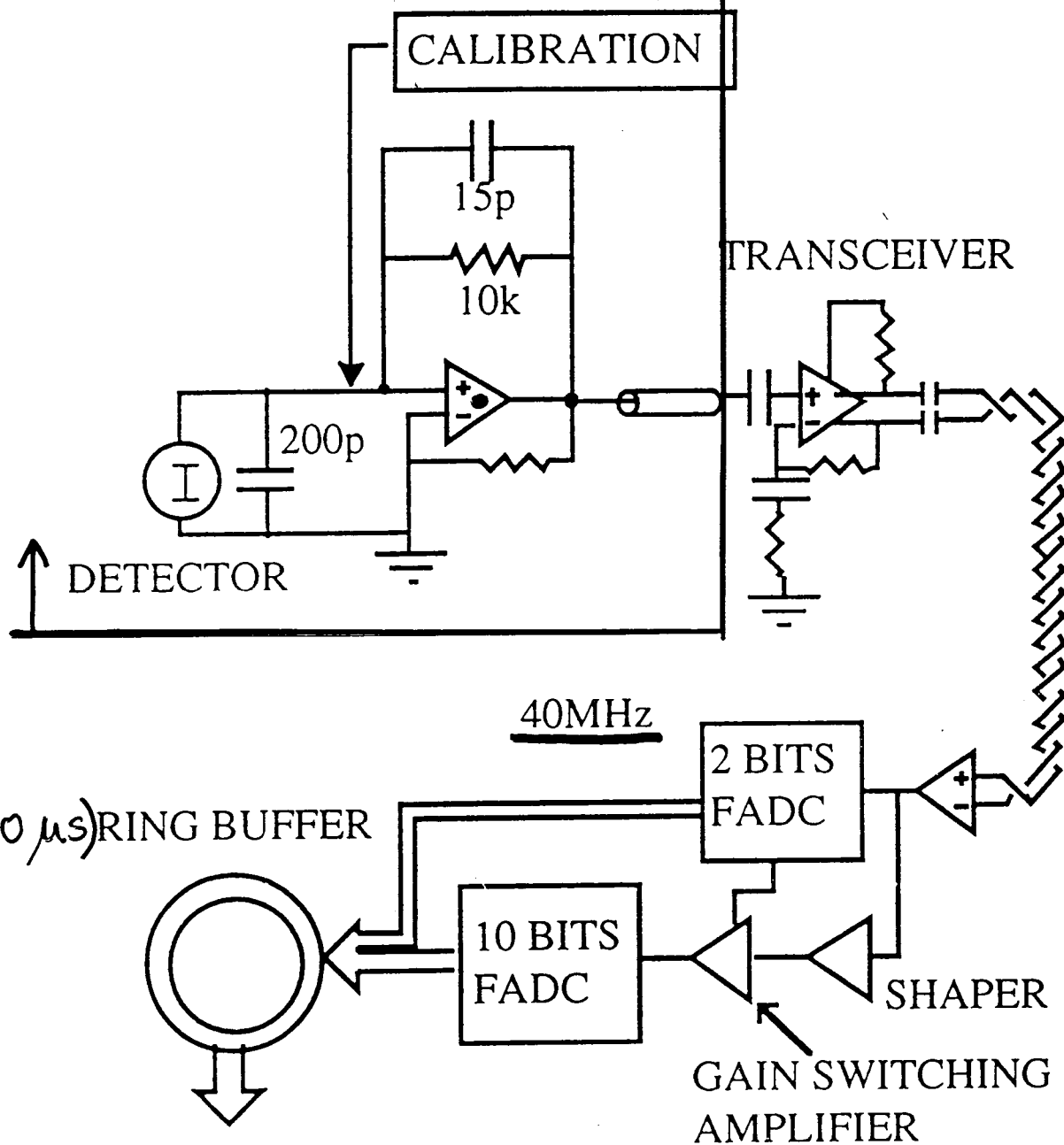
THE FRONT END ELECTRONICS

- THE PREAMPS AND THE CALIBRATION SYSTEM ELECTRONICS ARE PLUGGED ON THE BACK → END OF RIBBONS, INSIDE THE LKr TO:
 - MINIMIZE THE NOISE (SI JFET'S ARE CLOSE TO THEIR MINIMUM NOISE FIGURE @ LKr $T = 120$ K)
 - EN. EQUIV. NOISE FROM 4 MeV → 8 MeV (@ 5 KV)
WITH SHAP. TIME 120 ns → 70 ns
 - EXPLOIT LKr BATH AS THERMOSTAT TO STABILIZE IN TEMPERATURE THE ABOUT 2000 PULSER GEN. OF THE CALIBR. SYSTEM
- CALIBRATION PULSES ARE PRODUCED LOCALLY TO AVOID DISTORSION OR CROSS-TALKS DUE TO TRANSMISSION OVER LONG LINES
- THE CALIBRATION SYSTEM IS IMPLEMENTED ON AN 18 LAYER MOTHER BOARD WHICH ALSO DISTRIBUTES THE P.S. TO 64 PREAMP CARDS
- THE PRECISION AND THE STABILITY OF THE CALIB. SYSTEM SHOULD ALLOW TO CONTROL THE RESPONSE UNIFORMITY OF THE ~ 13500 CH. TO BETTER THAN 0,5 % (THE FINAL CHECK IS NOW POSSIBLE WITH ALL FADC'S INSTALLED)



ELECTRONICS CHAIN

© LKr TEMPERATURE ←



- PREAMP BNL - RADEKA TYPE
(CHARGE INTEGRATING, Si JFET)

• PROBLEM: A FEW CAP'S ARE DISCHARGING

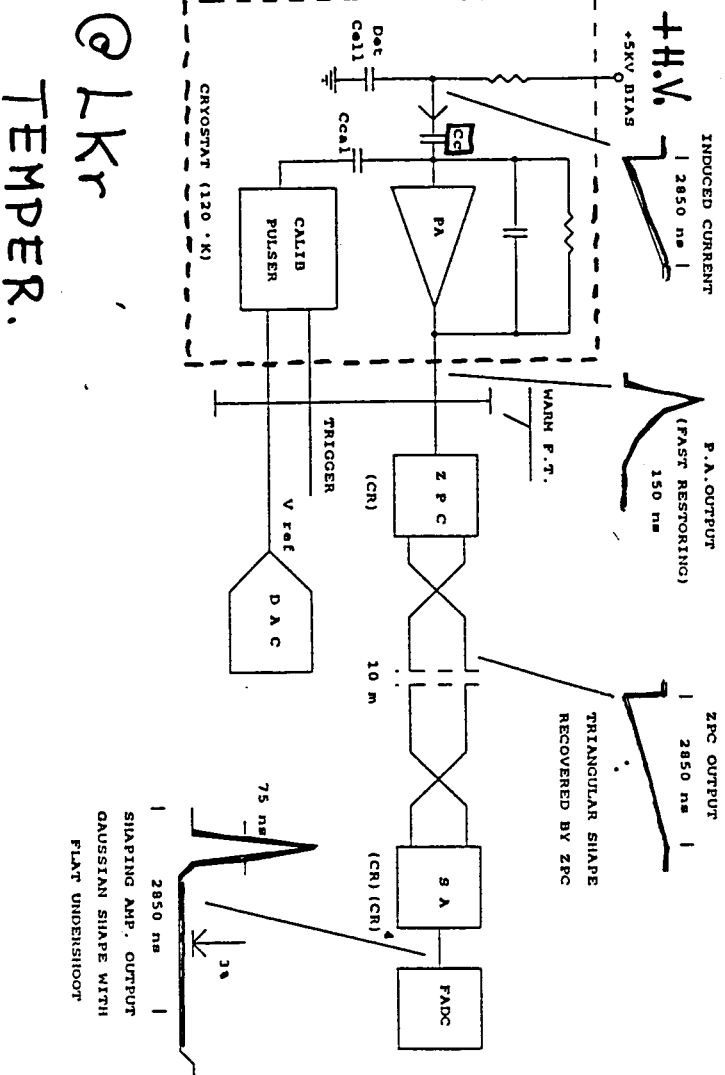
@ ≈ 2 KV

• LIKELY WE'LL REPLACE ALL CAPACITORS DURING WINTER SHUT DOWN

• THE MAIN EFFECT IS A $\approx 0.2\%$ CORRECTION DUE TO SPACE CHARGE EFFECT

• THIS CORRECTION HAS TO BE APPLIED AT NOMINAL INTENSITY(*) IN THE 2-nd HALF OF 2.4 S SPS SPILL

(*) $1.4 \cdot 10^6$ K DECAYS IN'S. DET.

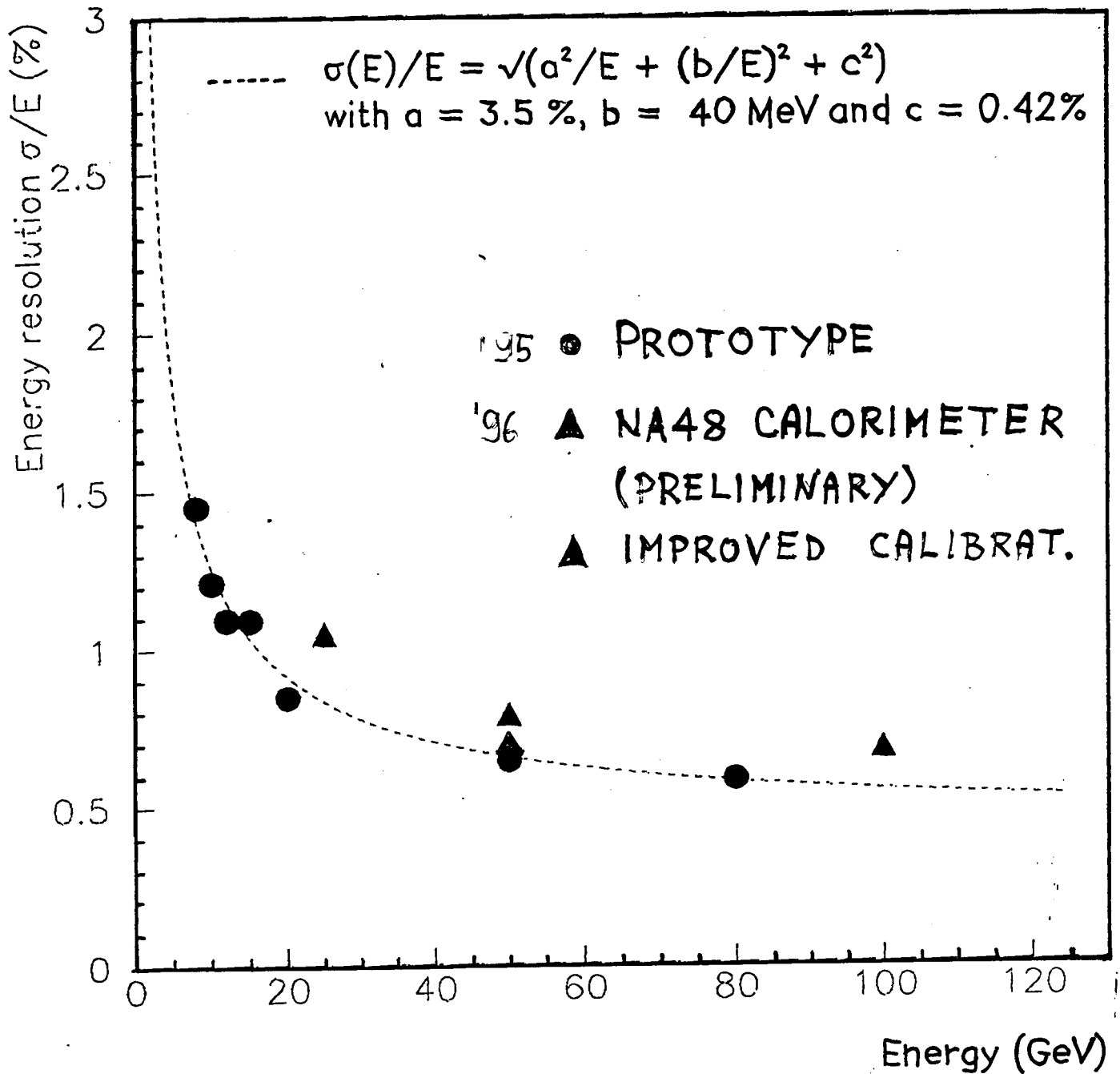


@ LKr
TEMPER.

□ H.V. DECOUPLING CAPACITOR

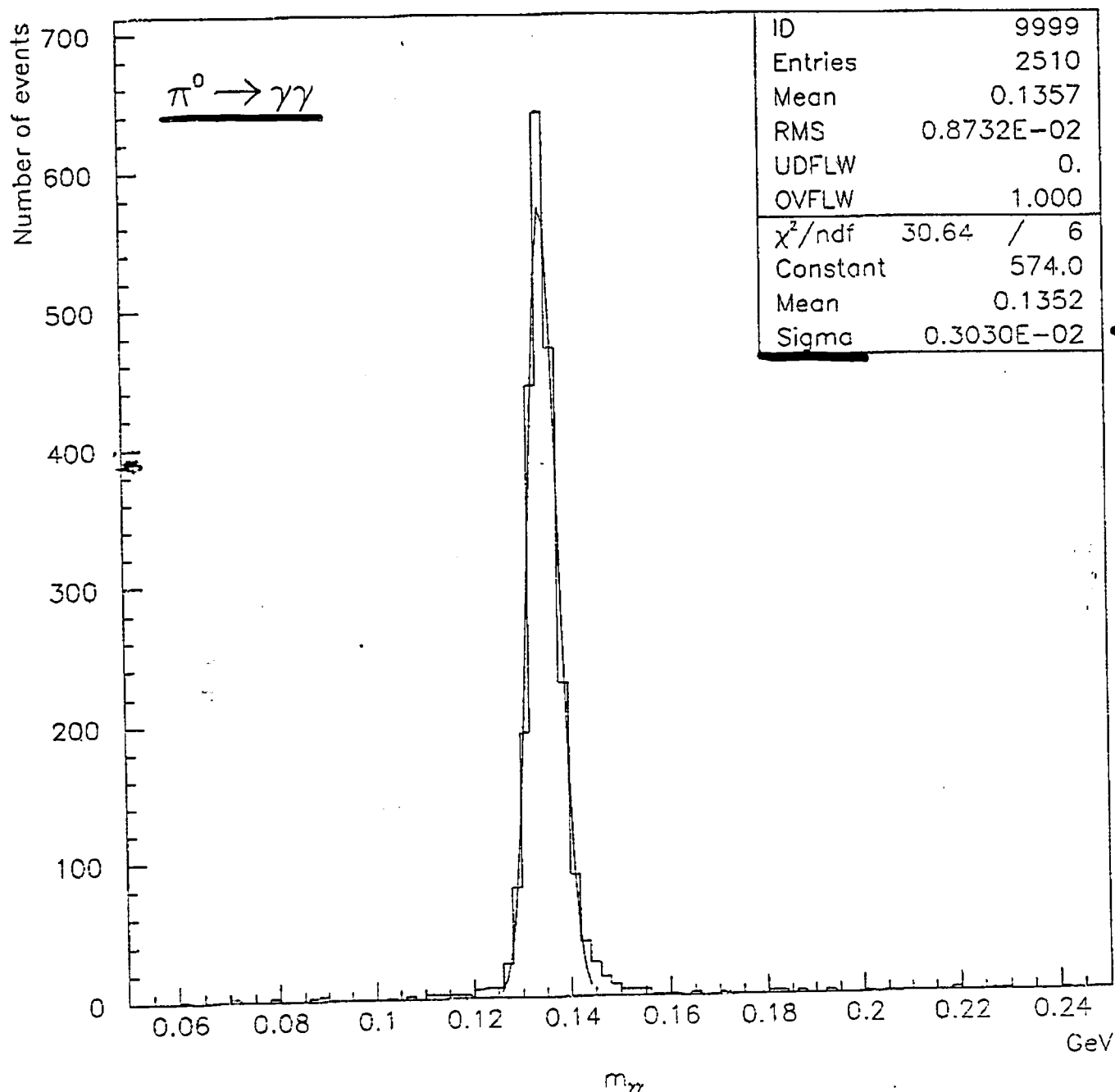
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NA48 PRELIMINARY



	▲ CALO '96	● PROTOT.
H.V. (kV)	1.5	5.0
SH. TIME (ns)	70	120
ELECTR.	FADC	ADC
PHASE CORR.	NO	YES

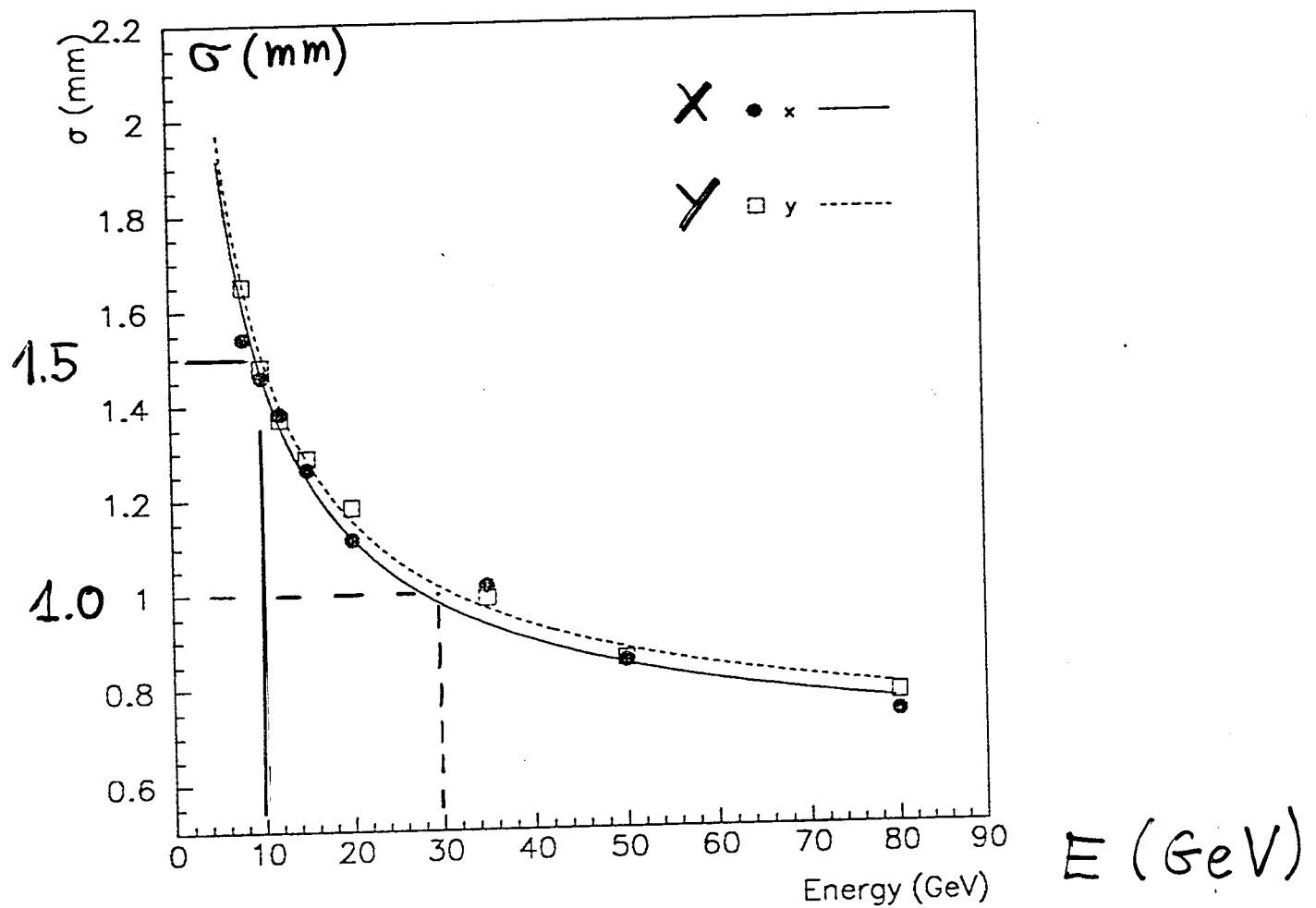
NA48 PRELIMINARY



- 96 DATA OBTAINED GROUPING 16 CELLS (2×8)
- IN THIS YEAR DATA CELLS ARE INDIVIDUALLY READ
- EXPECTED RESOLUTION ~ 1 MeV

NA48 LKr CALORIMETER

POSITION RESOLUTION

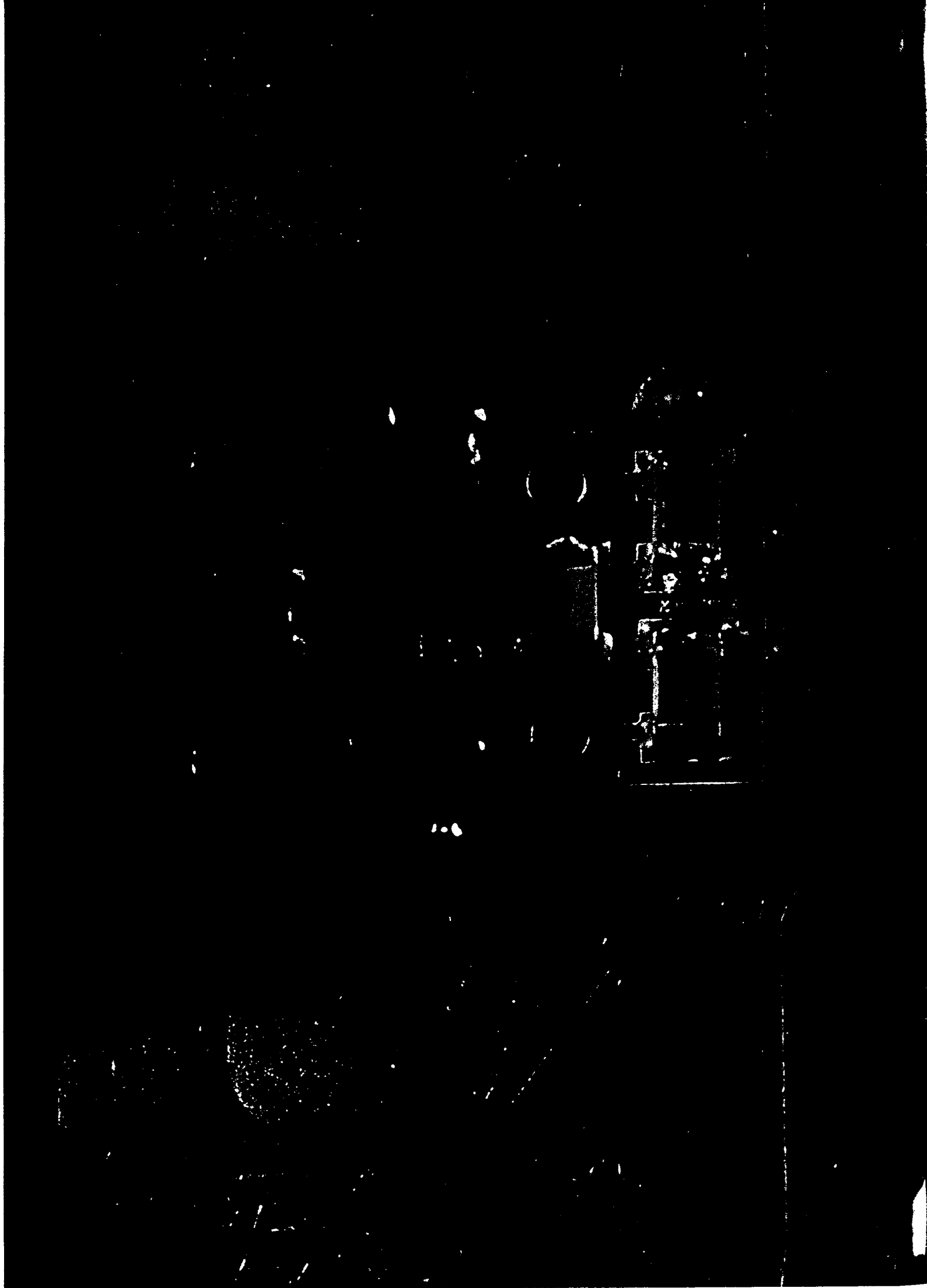


$$\sigma_x \approx \sigma_y = (4.2/\sqrt{E} + 0.6) \text{ mm}$$

- PRELIMINARY RESULTS OF CALORIMETER
~ MATCH PROTOTYPE ONES.

THE PREAMPLIFIER PROTECTION SYSTEM DURING H.V. CONDITIONING

- THE SYSTEM AIM IS TO PREVENT PREAMPS, FROM BEING DAMAGED BY POSSIBLE H.V. DISCHARGES BTW. RIBBONS DURING THE INITIAL H.V. RAMP-UP AND CONDITIONING
- IN THE 'CLOSED' POSITION OF THIS SWITCHING SYSTEM ALL PREAMPS INPUTS ARE SIMULTANEOUSLY GROUNDED BY SETS OF LONG METALLIC SPRING CONTACTS.
- TESTS HAD SHOWN THAT CONTINUOUS H.V. DISCHARGES UP TO 7 KV 'SIMULATED' IN THE RIBBON STRUCTURE
LEAVE PREAMPS UNAFFECTED.
- THE SWITCHING MECHANICAL ACTION INSIDE THE CRYOSTAT, IS OBTAINED BY A SET OF 64 BELLOW PAIRS DRIVEN BY A GAS CONTROLLED SYSTEM PLACED OUTSIDE THE CRYOSTAT



CONCLUSIONS

- PRELIMINARY RESULTS ON '96 DATA
~ MATCH PROTOTYPE ONES

ENERGY

$$\sigma(E)/E = \frac{3.5\%}{\sqrt{E}} + \frac{0.04}{E} + 0.4\%$$

POSITION

$$\sigma_x \approx \sigma_y = \frac{4.2}{\sqrt{E}} + 0.6 \text{ mm}$$

TIME

$$\sigma_T = \frac{0.6}{\sqrt{E}} + \frac{1.7}{E} + 0.2 \text{ ns}$$

- FINAL RESULTS FROM '97 DATA WITH INDIVIDUAL CELL READ-OUT
('96 DATA TAKEN READING OVER THE ENTIRE CALORIMETER GROUPS OF 16 CELLS 2×8)
- H.V. PROTECTION SYSTEM WORKS WELL.